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(54) Title: PROCESS FOR THE MANUFACTURE OF DICHLOROPROPANOL

(57) Abstract: Process for manufacturing dichloropropanol via reaction between glycerol and/or monochloropropanediol and a chlorinating agent in a reactor which is supplied with one or more liquid streams, in which the sum of the glycerol and monochloropropanediol contents in all the liquid streams introduced into the reactor is less than 50 wt% and in which all the liquid streams introduced into the reactor comprise at least one liquid recycling stream, the recycling stream forming at least 10 wt% of all the liquid streams introduced into the reactor.



WO 2008/107468 A1

Process for the manufacture of dichloropropanol

The present patent application claims the benefit of the patent application FR 0753689 filed on 7 March 2007, and of the provisional US patent application 61/013680 filed on 14 December 2007, the content of both of which is incorporated here by reference.

5 The present invention relates to a process for manufacturing dichloropropanol. The present invention relates more specifically to a process for manufacturing dichloropropanol via reaction between glycerol and/or monochloropropanediol and a chlorinating agent.

10 Dichloropropanol is a reaction intermediate in the manufacture of epichlorohydrin and epoxy resins (*Kirk-Othmer Encyclopedia of Chemical Technology*, Fourth Edition, 1992, Vol. 2, page 156, John Wiley & Sons, Inc.).

15 According to known processes, dichloropropanol can be obtained in particular by hypochlorination of allyl chloride, by chlorination of allyl alcohol and by hydrochlorination of glycerol. The latter process exhibits the advantage that the dichloropropanol can be obtained starting from fossil raw materials or renewable raw materials and it is known that petrochemical natural resources, from which the fossil materials originate, for example oil, natural gas or coal, available on Earth are limited.

20 International Application WO 2005/021476 describes a process for manufacturing dichloropropanol via reaction between glycerol and/or monochloropropanediol and gaseous hydrogen chloride in the presence of acetic acid as a catalyst. The glycerol and/or monochloropropanediol content in the entirety of the liquid supply of the reactor is at least 50 wt%. The entirety of the supply comprises a recycling stream. In this process, undesirable products are
25 formed and collected as residues in a tank.

The present invention aims to solve this problem by providing a novel process which limits the formation of undesirable by-products without however decreasing the selectivity of the reaction for dichloropropanol.

30 The invention hence relates to a process for manufacturing dichloropropanol via reaction between glycerol and/or monochloropropanediol and a chlorinating agent in a reactor which is supplied with one or more liquid streams, in which the sum of the glycerol and monochloropropanediol contents

in all the liquid streams introduced into the reactor is less than 50 wt% and in which all the liquid streams introduced into the reactor comprise at least one liquid recycling stream, the recycling stream forming at least 10 wt% of all the liquid streams introduced into the reactor.

- 5 One of the main features of the present invention lies in the fact that the sum of the glycerol and monochloropropanediol contents in all the liquid streams that supply the glycerol chlorination reactor is less than 50 wt%. This makes it possible to reduce the amount of undesirable by-products. An additional advantage of this procedure is in tolerating a greater content of by-products in
10 the reactor with, as a result, a concomitant decrease of the purge flow from the reactor and of the concentration of recoverable products in the purge flow, and therefore a reduction in the size of the installations for treating the purges. All these advantages contribute to a reduction in the overall cost of the process. Furthermore, this also makes it possible to reduce the reaction volume. As the
15 reactions are balanced, it is thus possible to increase the rate of dichloropropanol synthesis by ensuring an effective removal of the latter from the reaction medium, in order to maintain a low concentration of dichloropropanol. This requires removing a large amount of the reaction medium, separating the dichloropropanol from the rest of the constituents of the reaction medium and
20 recycling the rest of the reaction medium. These two joint operations, that is to say the removal of dichloropropanol and keeping a greater content of by-products in the reactor may be expressed by the glycerol and monochloropropanediol content of all the liquid streams that supply the glycerol chlorination reactor.
- 25 Another of the main features of the present invention lies in the fact all the liquid streams introduced into the reactor comprise at least one liquid recycling stream, the recycling stream forming at least 10 wt% of all the liquid streams introduced into the reactor. Such a recycling stream has several advantages. Firstly, it helps to lower the sum of the glycerol and monochloropropanediol
30 contents in all the liquid streams that supply the glycerol chlorination reactor to less than 50 wt% without introducing external compounds and the need to recycle and dispose of such compounds. External compounds do not comprise the reactants used and the products formed during the chlorination reaction. Solvents are examples of external compounds. Secondly, such a recycling
35 stream allows reducing the purge flow from the reactor, and therefore a reduction

in the size of the installations for treating the purges. All these advantages contribute to a reduction in the overall cost of the process.

The expression "liquid stream that supplies the chlorination reactor" is understood to mean any stream of material that is liquid at the temperature for introduction into the reactor, and which is introduced into the reactor. These liquid streams may contain various compounds such as, for example, glycerol, monochloropropanediol and the chlorinating agent, impurities present in the glycerol, monochloropropanediol and chlorinating agent, an organic solvent, water, a catalyst for the reaction, reaction intermediates and products and by-products of the reaction.

The expression "liquid recycling stream" is understood to mean any stream of material derived from at least one step of the dichloropropanol manufacturing process located downstream of the reactor, which is liquid at the temperature for introduction into the reactor, and which is introduced into the reactor.

This step of the process downstream of the reactor may be a physical or chemical treatment step. Among the physical treatment steps, mention may, for example, be made of the operations for separation via stripping, distillation, evaporation, extraction, settling, centrifugation, precipitation, filtration and adsorption. Among the chemical treatment steps, mention may, for example, be made of a hydrolysis treatment intended to recover an optional catalyst and a transesterification treatment intended to recover the dichloropropanol and the catalyst.

The removal of water from the reaction medium via distillation of an azeotropic water/dichloropropanol mixture is an example of a physical treatment step downstream of the reactor. The liquid return stream of the distillation column is considered to be a recycling stream. The distillation system may be located on top of the chlorination reactor or in an external circulation loop of the reaction mixture.

In the process according to the invention, the liquid recycling stream forms at least 10 wt% of all the liquid streams introduced into the reactor, preferably at least 20 wt%, more preferably at least 50 wt%, even more preferably at least 90 wt% and most particularly preferably at least 95 wt%. The recycling stream forms at most 99 wt% of all the liquid streams introduced into the reactor, and particularly preferably at most 97.5%.

The process according to the invention may be carried out in batch, semi-continuous or continuous mode. Continuous mode is preferred.

In the process according to the invention, the liquid recycling stream generally comprises at least one of the following compounds: glycerol, monochloropropanediol, the chlorinating agent, a carboxylic acid, a carboxylic acid salt, an inorganic salt, a glycerol ester, a polyester of glycerol, a
5 monochloropropanediol ester, a poly ester of monochloropropanediol, water, a catalyst, a solvent, dichloropropanol, a dichloropropanol ester, a glycerol oligomer, a partially chlorinated and/or esterified glycerol oligomer.

In the process according to the invention, the liquid recycling stream generally comprises from 0.01 to 25 wt% of glycerol, preferably from 0.1 to
10 20 wt%, more preferably from 0.2 to 15 wt% and most particularly preferably from 0.3 to 10 wt%.

In the process according to the invention, the liquid recycling stream generally comprises from 0.01 to 40 wt% of glycerol esters, preferably from 0.05 to 30 wt%, more preferably from 0.1 to 20 wt% and most particularly preferably
15 from 0.2 to 15 wt%.

In the process according to the invention, the liquid recycling stream generally comprises from 0.1 to 70 wt% of monochloropropanediol, preferably from 0.5 to 60 wt%, more preferably from 1 to 50 wt% and most particularly preferably from 6 to 49 wt%.

20 In the process according to the invention, the liquid recycling stream generally comprises from 5 to 90 wt% of monochloropropanediol esters, preferably from 10 to 85 wt%, more preferably from 20 to 82 wt% and most particularly preferably from 25 to 80 wt%.

In the process according to the invention, the liquid recycling stream
25 generally comprises from 0.1 to 60 wt% of partially chlorinated and/or esterified glycerol oligomers, preferably from 0.2 to 50 wt%, more preferably from 1 to 45 wt% and most particularly preferably from 2 to 40 wt%.

The glycerol in the process according to the invention may be obtained starting from fossil raw materials or starting from renewable raw materials,
30 preferably starting from renewable raw materials.

The expression "fossil raw materials" is understood to mean materials derived from the treatment of petrochemical natural resources, for example oil, natural gas and coal. Among these materials, organic compounds that consist of a number of carbon atoms which is a multiple of 3 are preferred. Allyl chloride,
35 allyl alcohol and "synthetic" glycerol are particularly preferred. The term

"synthetic" glycerol is understood to mean a glycerol generally obtained from petrochemical resources.

The expression "renewable raw materials" is understood to mean materials derived from the treatment of renewable natural resources. Among these materials, "natural" glycerol is preferred. "Natural" glycerol may, for example, be obtained by conversion of sugars via thermochemical processes, these sugars possibly being obtained starting from biomass, as described in "Industrial Bioproducts: Today and Tomorrow, Energetics, Incorporated for the U.S. Department of Energy, Office of Energy Efficiency and Renewable Energy, Office of the Biomass Program, July 2003, pages 49, 52 to 56". One of these processes is, for example, catalytic hydrogenolysis of sorbitol obtained by thermochemical conversion of glucose. Another process is, for example, catalytic hydrogenolysis of xylitol obtained by hydrogenation of xylose. Xylose may, for example, be obtained by hydrolysis of hemicellulose contained in maize fibres. The expressions "natural glycerol" or "glycerol obtained from renewable raw materials" are understood to mean, in particular, glycerol obtained during the manufacture of biodiesel or else glycerol obtained during conversions of fats or oils of vegetable or animal origin, in general such as saponification, transesterification or hydrolysis reactions.

Among the oils that can be used to manufacture natural glycerol, mention may be made of all common oils, such as palm, palm kernel, coconut, babassu, old or new rapeseed, sunflower, maize, castor and cottonseed oils, arachis, soybean, linseed and sea kale oils and all the oils derived from, for example, sunflower or rapeseed plants obtained by genetic modification or hybridization.

Use can even be made of used frying oils, various animal oils, such as fish oils, tallow, lard and even abattoir fats.

Among the oils used, mention may also be made of oils partially modified, for example, by polymerization or oligomerization such as, for example, the "stand oils" of linseed and sunflower oils and blown vegetable oils.

A particularly suitable glycerol may be obtained during the conversion of animal fats. Another particularly suitable glycerol may be obtained during the manufacture of biodiesel. Another particularly suitable glycerol may be obtained during the fatty acid manufacture.

In one embodiment of the process according to the invention, a glycerol external to the process according to the invention is used. The term "external"

glycerol is understood to mean glycerol which is not recycled in the process according to the invention.

In another embodiment of the process according to the invention, a mixture of glycerol "external" to the process according to the invention and of glycerol
5 "internal" to the process according to the invention is used. The term "internal" glycerol is understood to mean glycerol which has been separated from the reaction products formed in the process according to the invention and which has then been recycled in the process according to the invention.

The monochloropropanediol used in the process according to the invention
10 may be obtained by any route, for example by reaction between glycerol and the chlorinating agent or by hydrolysis of epichlorohydrin.

In a first embodiment variant of the process according to the invention, a monochloropropanediol extrinsic to the process according to the invention is used. The term "extrinsic" monochloropropanediol is understood to mean
15 monochloropropanediol which is not one of the products formed in the process according to the invention.

In a second embodiment variant of the process according to the invention, which is preferred, a monochloropropanediol intrinsic to the process according to the invention is used. The term "intrinsic" monochloropropanediol is understood
20 to mean monochloropropanediol which is one of the products formed in the process according to the invention, which has been separated from the other reaction products and which has then been recycled in the process according to the invention.

In the process according to the invention, the sum of the glycerol and
25 monochloropropanediol contents in all the liquid streams introduced into the reactor is preferably less than or equal to 49 wt%, more preferably less than or equal to 45 wt% and most particularly preferably less than or equal to 40 wt%. This content is generally greater than 1 wt%.

In the process according to the invention, the glycerol content in all the
30 liquid streams introduced into the reactor is preferably less than or equal to 49 wt%, more preferably less than or equal to 30 wt% and most particularly preferably less than or equal to 20 wt%. This content is generally greater than 1 wt%.

When the glycerol and monochloropropanediol are present in all the liquid
35 streams introduced into the reactor, the glycerol content in the mixture of glycerol and monochloropropanediol is generally greater than or equal to 1 wt%,

usually greater than or equal to 5 wt%. This content is generally less than or equal to 99.9 wt%, usually less than or equal to 90 wt%.

In the process according to the invention, the chlorinating agent generally comprises hydrogen chloride. The hydrogen chloride may be gaseous hydrogen chloride, an aqueous solution of hydrogen chloride or a mixture of the two,
5 preferably gaseous hydrogen chloride or a mixture of gaseous hydrogen chloride and an aqueous solution of hydrogen chloride.

In the process according to the invention, the reaction between glycerol and/or the chlorinating agent may be carried out in the presence of a catalyst,
10 preferably a carboxylic acid or a carboxylic acid derivative, and most particularly preferably adipic acid or an adipic acid derivative. The expression "carboxylic acid derivatives" is understood to mean carboxylic acid halides, carboxylic acid esters, carboxylic acid anhydrides, carboxylic acid amides and mixtures of at least two of them.

In the process according to the invention, it is possible to use an organic solvent, such as a chlorinated organic solvent, an alcohol, a ketone, an ester or an ether, a non-aqueous solvent that is miscible with glycerol and/or
15 chloropropanediol such as dioxane, phenol, cresol and dichloropropanol, or heavy products from the reaction, such as glycerol oligomers that are at least partially chlorinated and/or esterified.
20

In the process for manufacturing dichloropropanol according to the invention, the reaction between glycerol and/or chloropropanediol, and the chlorinating agent is preferably carried out in a liquid reaction medium. The liquid reaction medium may be single phase or multiphase.

25 The liquid reaction medium is formed by all the solid, liquid or gaseous compounds dissolved or dispersed at the reaction temperature.

The reaction medium generally comprises the reactants, catalyst, solvent, impurities present in the reactants, in the solvent and in the catalyst, reaction intermediates and products and by-products of the reaction.

30 The term "reactants" is understood to mean glycerol and/or monochloropropanediol, and the chlorinating agent. The monochloropropanediol may be 3-chloro-1,2-propanediol or 2-chloro-1,3-propanediol or a mixture of these two isomers.

35 Among the impurities present in the glycerol, mention may be made of carboxylic acids, carboxylic acid salts, of fatty acids esters such as mono-, di-

and triglycerides, fatty acids esters with alcohols used during transesterification, inorganic salts such as alkali and alkaline-earth metal chlorides and sulphates.

Among the reaction intermediates, mention may be made of monochloropropanediol and its esters and/or polyesters, esters and/or polyesters of glycerol and dichloropropanol esters.

The glycerol ester may therefore be, depending on the case, an impurity of the glycerol or a reaction intermediate.

The monochloropropanediol may be, depending on the case, a reactant or a reaction intermediate.

The expression "products of the reaction" is understood to mean dichloropropanol and water.

The dichloropropanediol may be 1,3-dichloro-2-propanol or 2,3-dichloro-1-propanol or a mixture of these two isomers.

The water may be water formed in the chlorination reaction and/or water introduced into the process, for example via the glycerol and/or the chlorinating agent.

Among the by-products, mention may be made, for example, of partially chlorinated and/or esterified glycerol oligomers.

The reaction intermediates and the by-products may be formed in the various steps of the process, such as for example, during the dichloropropanol manufacturing step and during the steps for separating the dichloropropanol.

In the process according to the invention, when the reactor is supplied by a liquid stream, this stream comprises the streams of reactants, catalyst, solvent and the recycling stream or streams.

In the process according to the invention, when the reactor is supplied by several liquid streams, these streams comprise the streams of reactants, catalyst and solvent, and recycling streams and mixtures thereof, and one of the streams is composed solely of a recycling stream.

In the process according to the invention, the reaction between glycerol and/or monochloropropanediol and the chlorinating agent is carried out at a temperature generally greater than or equal to 70°C, preferably greater than or equal to 90°C and most particularly preferably greater than or equal to 110°C. This reaction temperature is generally less than or equal to 160°C, preferably less than or equal to 150°C and most particularly preferably less than or equal to 140°C.

In the process according to the invention, the reaction between glycerol and/or monochloropropanediol and the chlorinating agent is carried out at a partial pressure of hydrogen chloride generally greater than or equal to 0.002 bar, preferably greater than or equal to 0.02 bar and most particularly preferably
5 greater than or equal to 0.05 bar. This pressure is generally less than or equal to 50 bar, preferably less than or equal to 30 bar and most particularly preferably less than or equal to 20 bar.

In one embodiment of the process according to the invention, the content of hydrogen chloride in the liquid reaction medium relative to the sum of the water and hydrogen chloride contents in the liquid reaction medium is generally
10 less than or equal to 20 wt%, preferably less than or equal to 17 wt% and more particularly preferably less than or equal to 15 wt%.

In another embodiment of the process according to the invention, the content of hydrogen chloride in the liquid reaction medium relative to the sum of
15 the water and hydrogen chloride contents in the liquid reaction medium is generally greater than or equal to 20 wt%, preferably greater than or equal to 30 wt% and more particularly preferably greater than or equal to 40 wt%.

The invention also relates to a process for manufacturing epichlorohydrin comprising the process for manufacturing dichloropropanol followed by a
20 process for the dehydrochlorination of dichloropropanol.

The epichlorohydrin obtained by dehydrochlorination of dichloropropanol may be used in the manufacture of epoxy resins.

The invention finally relates to a process for manufacturing epoxy resins, in which epichlorohydrin, at least one part of which was obtained in the process
25 for manufacturing epichlorohydrin according to the invention, is subjected to a reaction with at least one compound containing at least two active hydrogen atoms. These compounds comprise polyphenols, monoamines and diamines, aminophenols, heterocyclic imides and amides, diols including ethylene glycol and propylene glycol and aliphatic polyols, and fatty acid dimers. In the process
30 for manufacturing epoxy resins, another part of the epichlorohydrin may be obtained by a process other than the dehydrochlorination of dichloropropanol derived from the chlorination of glycerol, such as a process for dehydrochlorination of dichloropropanol derived from hypochlorination of allyl chloride, a process for dehydrochlorination of dichloropropanol derived from
35 chlorination of allyl alcohol, or an allyl chloride epoxidation process.

The epoxy resins thus obtained may be used in coating applications and in structural applications. The coating applications relate to the fields of maritime transport and of industrial maintenance (anticorrosion primer paints for metal and concrete structures), of coatings for metallic containers (food preserves, cans
5 for drinks, drums, buckets and aerosol bottles) and for windings, of motor vehicle coatings (primers), of inks and masks for electronic circuits. The structural applications relate to the fields of structural composites (epoxy resin composites with glass, boron, carbon and aromatic polyamide fibres), of civil engineering, of floor covering (paints for coating floors, parquet, paving, tiling,
10 self-levelling coatings, roughcast floors, tempered floors, floor coverings for cold rooms), of construction, of electrical equipment (sealing of electrical and electromechanical devices such as battery housings, resistors, fuses, thermal circuit breakers, cable joints, windings) and of electronic equipment (coatings and laminated sheets for printed circuits and encapsulation of printed circuits), of
15 adhesives (bonding of different materials such as metals, glass, ceramics, wood, concrete, plastics) and of tooling (prototypes, master patterns, moulds and other parts) for the aerospace, automotive, foundry and maritime construction industries.

Epoxy resins also find applications in the fields of energy (wind energy),
20 of aeronautics (honeycomb sandwich panels, helicopter rotor blades, cowls and engine nacelles, flaps, ailerons, rudders) and of fluid (gas, oil) transport.

The example below is intended to illustrate the invention without, however, limiting it.

Example 1 (according to the invention)

25 Figure 1 represents one particular scheme of an installation which has been used to apply the dichloropropanol production process according to the invention.

A reactor (4) was continuously supplied, at 130°C and at atmospheric pressure, with glycerol via the line (1) and a 34 wt% aqueous solution of
30 hydrogen chloride via the line (2). A distillation column (6) was supplied via the line (5) with a gas phase produced by the reactor (4); the residue from the column (6) was recycled via the line (8) to the reactor (4). The production stream (7) contains most of the water produced by the process and a first part of the dichloropropanol production. A liquid purge was drawn off from the
35 reactor (4) via the line (9) and supplied an evaporator (10) where an operation of partial evaporation of the mixture was carried out by heating; the gas phase

which contains most of the hydrogen chloride and the water from the stream (9) was recycled via the line (11) to the bottom of the column (6). A stripping column (13) was supplied by the liquid phase coming from the evaporator (10) via the line (12) and by a stream of nitrogen introduced via the line (16); a
5 second part of the dichloropropanol production was collected at the top of the column (13) via the line (14) and the residue from the column (13) was recycled to the reactor (4) via the line (15). A purge of the reaction mixture from the reactor (4), in which the heavy by-products of the reaction, such as chlorinated glycerol oligomers, accumulated, was carried out in batch mode via the
10 line (17). The amount of catalyst removed from the reactor via the purge was compensated for by an addition of catalyst via the line (3). The weight proportions of glycerol introduced into the reactor (4) via the lines (1) and (15) and of glycerol monochlorohydrin introduced via the line (15) were respectively equal to 3.9% and 14.1% of the total of the liquid streams supplying the reactor
15 via the lines (1), (2), (8) and (15). The recycling stream which supplied the reactor (4) via the lines (8) and (15) was 90% of all of the liquid streams introduced into the reactor (4).

Example 2 (not according to the invention)

Aqueous hydrochloric acid with a concentration of 4 mol of hydrogen
20 chloride/kg of solution (96.8 g/h), glycerol (22 g/h) and caprylic acid (6.37 g/h) have been introduced at a constant flow rate into a 350 ml glass reactor thermostatted at a temperature of 120 °C. The reactor, which functioned at atmospheric pressure, was equipped with an overflow system for maintaining a constant volume of liquid. The reaction mixture fraction that was vaporized was
25 evacuated from the reactor and condensed at ambient temperature. The condensate separated into 2 phases: a dense organic phase containing mainly dichloropropanol and a lighter aqueous phase containing most of the hydrochloric acid which had not reacted. The liquid mixture collected at the overflow outlet contained the remainder of the dichloropropanol production. No
30 flow was recycled to the reactor. The process was operated during 25 h to equilibration. The global dichloropropanol productivity estimated from the flows and the compositions of the condensate and the overflow outlet was 26.4 g dichloropropanol/h/l.

Example 3 (according to the invention)

35 Aqueous hydrochloric acid with a concentration of 4 mol of hydrogen chloride/kg of solution (98.7 g/h), glycerol (22 g/h) and caprylic acid (6.21 g/h)

have been introduced at a constant flow rate into a 350 ml glass reactor thermostatted at a temperature of 119.4 °C. The reactor, which functioned at atmospheric pressure, was equipped with an overflow system for maintaining a constant volume of liquid. The reactor was surmounted by a distillation column
5 for rectifying the reaction medium fraction vaporized. The reflux to the column was adjusted so that a flow of 155 g/h of liquid was returned from the distillation column to the reactor. The mixture exiting the top of the distillation column was condensed at ambient temperature. The condensate separated into 2 phases: a
10 dense organic phase containing mainly dichloropropanol and a lighter aqueous phase containing most of the hydrochloric acid which had not reacted. The liquid mixture collected at the overflow outlet contained the remainder of the dichloropropanol production. The global dichloropropanol productivity estimated from the flows and the compositions of the condensate and the overflow outlet after equilibration was 46 g dichloropropanol/h/l.

CLAIMS

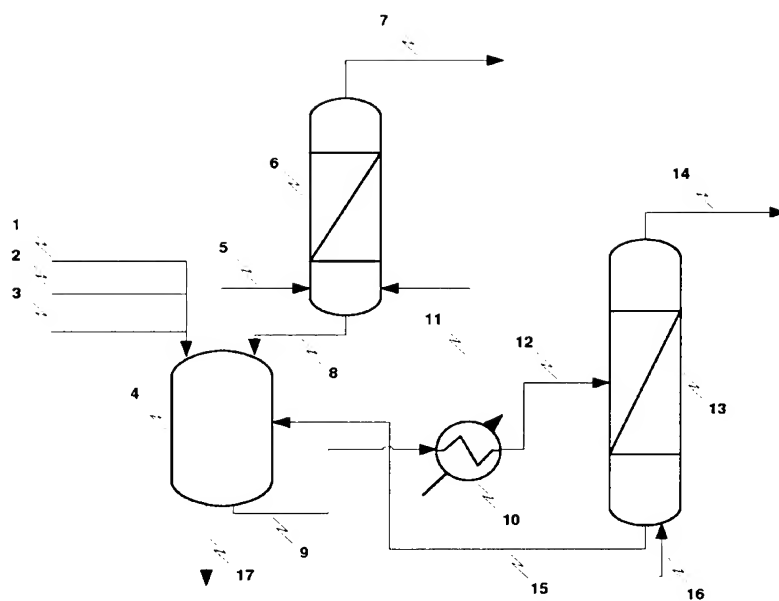
- 1 – Process for manufacturing dichloropropanol via reaction between glycerol and/or monochloropropanediol and a chlorinating agent in a reactor which is supplied with one or more liquid streams, in which the sum of the glycerol and monochloropropanediol contents in all the liquid streams introduced into the reactor is less than 50 wt% and in which all the liquid streams introduced into the reactor comprise at least one liquid recycling stream, the recycling stream forming at least 10 wt% of all the liquid streams introduced into the reactor.
- 2 – Process according to Claim 1, in which the liquid recycling stream forms at least 20 wt% and at most 99 wt% of all the liquid streams introduced into the reactor.
- 3 – Process according to Claim 1 or 2, in which the reactor is supplied in continuous mode.
- 4 – Process according to any one of Claims 1 to 3, in which the liquid recycling stream comprises at least one of the following compounds: glycerol, monochloropropanediol, the chlorinating agent, a salt, a glycerol ester, a monochloropropanediol ester, water, a catalyst, a solvent, dichloropropanol, a dichloropropanol ester, a glycerol oligomer, a chlorinated and/or esterified glycerol oligomer.
- 5 – Process according to any one of Claims 1 to 4, in which the recycling stream contains from 0.01 to 25 wt% of glycerol.
- 6 – Process according to any one of Claims 1 to 5, in which the recycling stream contains from 0.1 to 70 wt% of monochloropropanediol.
- 7 – Process according to any one of Claims 1 to 6, in which the sum of the glycerol and monochloropropanediol contents in all the liquid streams introduced into the reactor is less than or equal to 40 wt%.
- 8 – Process according to any one of Claims 1 to 7, in which the glycerol is obtained starting from renewable raw materials and in which the chlorinating

agent contains gaseous hydrogen chloride or a mixture of gaseous hydrogen chloride and an aqueous solution of hydrogen chloride.

9 – Process according to any one of Claims 1 to 8, followed by manufacture of epichlorohydrin by dehydrochlorination of dichloropropanol.

- 5 10 – Process according to Claim 9, in which the epichlorohydrin is involved in the manufacture of epoxy resins.

Figure 1



INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2008/052711

A. CLASSIFICATION OF SUBJECT MATTER
INV. C07C29/62

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
C07C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, BEILSTEIN Data, CHEM ABS Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	WO 2006/100314 A (SOLVAY [BE]; KRAFFT PHILIPPE [BE]; GILBEAU PATRICK [BE]; BALTHASART DO) 28 September 2006 (2006-09-28) claims 1,13-15 figure 1 page 25, lines 14,31,32 -----	1-10
Y	US 2 144 612 A (BRITTON EDGAR C ET AL) 24 January 1939 (1939-01-24) page 2; example 4 -----	1-10
Y	WO 2005/054167 A (SOLVAY [BE]; KRAFFT PHILIPPE [BE]; GILBEAU PATRICK [BE]; GOSSELIN BENO) 16 June 2005 (2005-06-16) example 12 figure 12 -----	1-10

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

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